

Uncertainties in THM-coupled integrity calculations

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Visit:

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OUTLINE

Parameter uncertainty in THM process – Feliks

Inhomogeneity and anisotropy in THM simulations – Aqeel

Additional slides (k1eme: C++ library for generating random fields – Charlie)

INTRODUCTION

Goals:

- Investigate if combining experimental data with modelling allows to gain insight to the effect of the thermo-osmosis process has impact on the pressurization.
- If an impact can be detected, quantify how big it is -> parameter estimation.

Uncertainties

- Parameter uncertainty
- Measurement uncertainty
- Inhomogeneity of clay
- Model uncertainty

What is thermo-osmosis?

TO is defined as follows:

"Thermo-osmosis may be defined as the process of diffusion of a fluid through a membrane under the influence of a temperature gradient" (Denbigh et al. 1952), (Gonçalvès et al. 2018)

- Fluid flow driven by a temperature gradient
- Unit: $\text{Pa} * \text{m} * \text{K}^{-1}$

INTRODUCTION - ATLAS EXPERIMENT

Geometry of experiment

- 2D, axisymmetric
- 100m x 119m
- Observation point at: (1.515, 14.0)

Numerical setup

- Processes:
 - Thermo Hydro Mechanical (THM)
 - Thermo Hydro Mechanical with thermo osmosis (THM+TO)
- Isotropy is assumed

Goals

- Match pressure and temperature observations
- Test if TO improves match between observed data and simulation

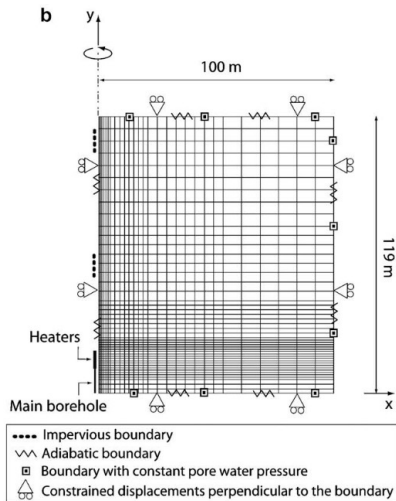


Fig. 1: Layout of ATLAS Experiment. Figure from: François et al. 2009

UNCERTAINTY QUANTIFICATION WORKFLOW

- Proxy building: parameter space was explored using numerical simulations based on Latin Hypercube Sampling (LHS) and 2-level-full-factorial experiment design
- Monte Carlo combined with proxies were used to explore parameter space with high saturation

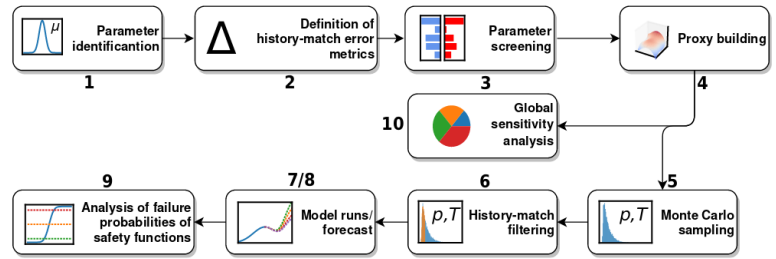


Fig. 2: Overview of the workflow used in this study. J. Buchwald et al. 2020

HYPOTHESIS TESTING

Goals:

- Test if TO has more impact than just being an arbitrary tweaking parameter
- Test if numerical method allow to select correct physical process
- Investigate how well the correct parameters can be recovered

Tab. 1: Table presenting an overview of tested process hypothesis. Each hypothesis is combination of a selection of a physical process and how thermo-osmosis is added to process. **Bold hypothesis** is the correct hypothesis in first experiment with no thermo-osmosis in reference data, *hypothesis in italics* is the correct hypothesis in the second experiment in which thermo-osmosis was included in the reference data.

Process	TO status	no TO	with TO	with TO active
	THM	THM	<i>THM+TO</i>	<i>THM+TO_active</i>
TRuni	TRuni	<i>TRuni+TO</i>	<i>TRuni+TO_active</i>	
TRhyd	TRhyd	<i>TRhyd+TO</i>	<i>TRhyd+TO_active</i>	

SIMULATION SETUP

Tested parameter ranges

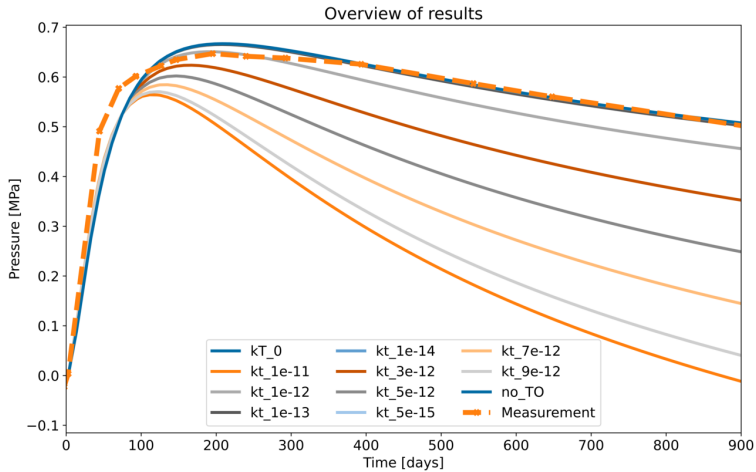
Parameter name	Unit	Reference	Min	Max
Intrinsic permeability (k)	m^2	$2.5e-19$	$1e-19$	$9e-19$
TO coefficient (narrow) (k_T)	$\text{Pa} * \text{m} * \text{K}^{-1}$	$3e-12$	$1e-12$	$5e-12$
TO coefficient (wide) (k_T)	$\text{Pa} * \text{m} * \text{K}^{-1}$	$3e-12$	$1e-14$	$1e-11$
Young's modulus (E)	Pa	$3.5e8$	$2e8$	$8e8$

Error metrics - History matching error:

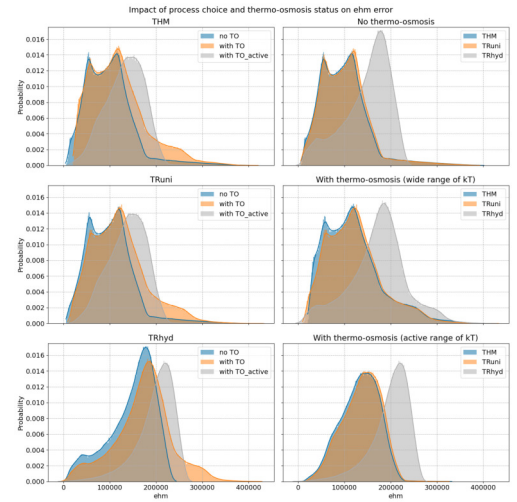
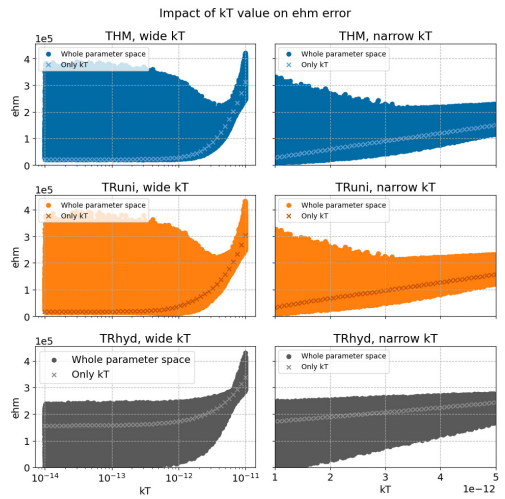
$$e_{HM} = \sqrt{\sum_1^n \frac{(d_{obs} - d_{sim})^2}{n}} \quad (1)$$

Parameters and initial conditions after: (Tamizdoust et al. 2021).

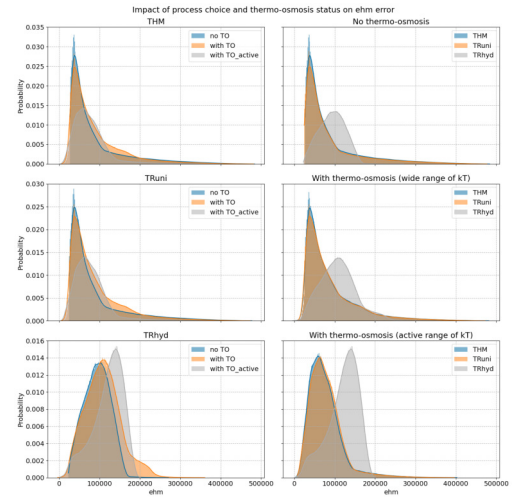
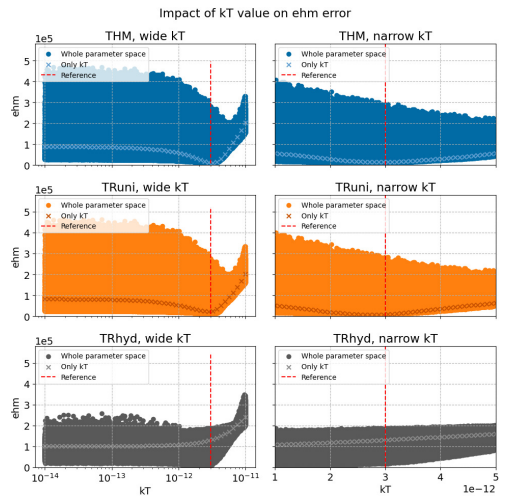
IMPACT OF THE VALUE OF K_T - TO COEFFICIENT



DISTRIBUTION OF ERROR VALUES - NO TO IN REFERENCE

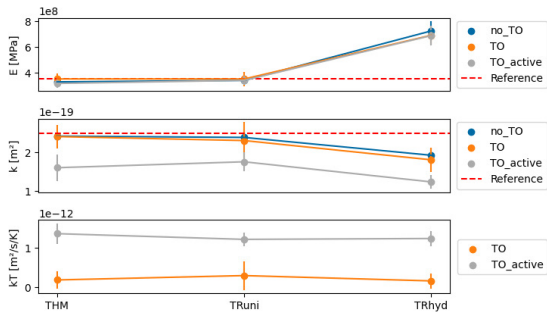


DISTRIBUTION OF ERROR VALUES - WITH TO IN REFERENCE

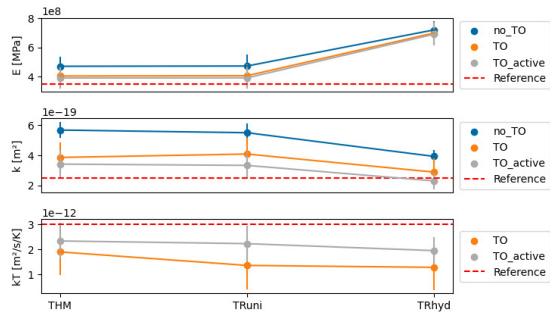


ESTIMATED PARAMETERS

Parameter values recovered
Reference data from THM



Parameter values recovered
Reference data from THM+TO(3e-12)



DISTRIBUTION OF PARAMETER VALUES

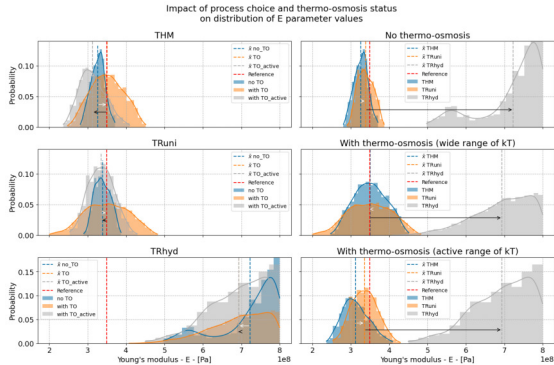


Fig. 3: Distribution of E values recovered with different processes with TO_active. No TO in the reference data.

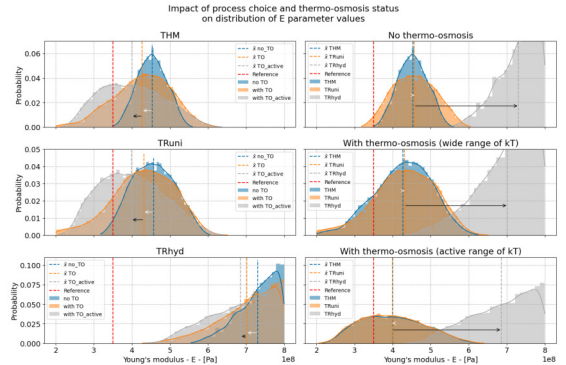


Fig. 4: Distribution of E values recovered with different processes with TO_active. With TO in the reference data.

DISTRIBUTION OF PARAMETER VALUES

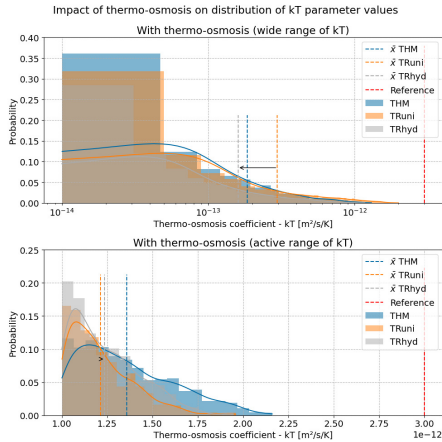


Fig. 5: Distribution of kT recovered with different processes with TO_{active} . No TO in the reference data.

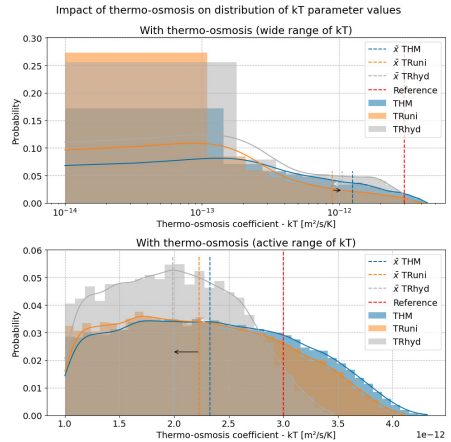


Fig. 6: Distribution of kT recovered with different processes with TO_{active} . With TO in the reference data.

SUMMARY AND OUTLOOK

Summary and conclusions:

- Increasing the complexity of the model doesn't necessarily improve the result
- The UQ tools can be used to discriminate between processes, select parameter values and quantify uncertainty

Outlook:

- Add information from multiple observations points
- Repeat the study presented in this presentation using data from real waste storage experiment
- Verify the significance of difference between the recovered distributions of parameter values with statistical methods

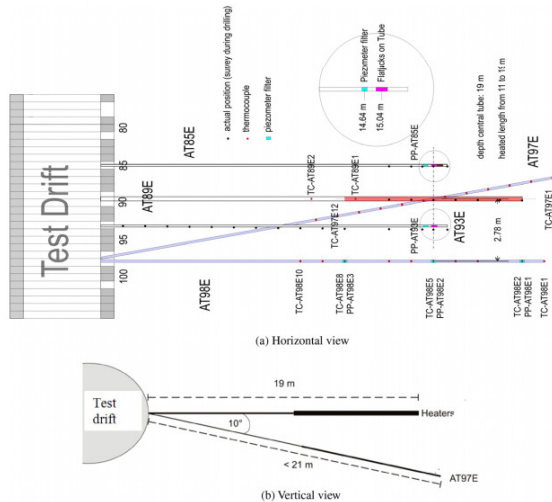
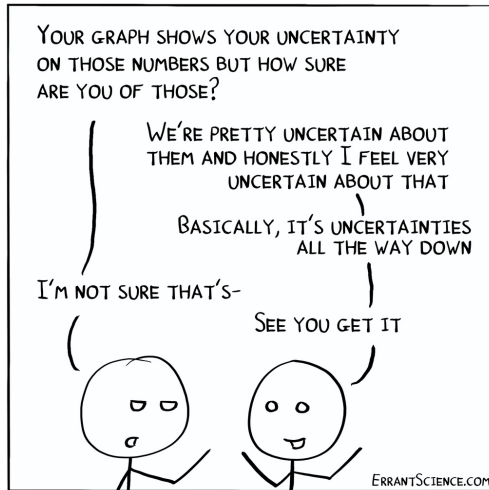


Fig. 1. Schematic view with instrumentation of the ATLAS III in situ test.

Fig. 7: ATLAS experiment - sensor positions (Chen et al. 2011)

COMICAL RELIEF AT THE END OF PRESENTATION :)



FLASHBACK – EXPECTED PLAN FOR MEQR

Starting point → FE experiment

Planned study steps

- Selection of input parameters for SA/UQ
→ based on knowledge from previous studies like Buchwald et al. 2020; Chaudhry et al. 2021
- Survey of available data sources (BGR)
→ parameter heterogeneities, (auto)correlation lengths
- Simplified 2D mesh/model based on FE experiment
- Use of as realistic data as possible from the original FE experiment
- Initial study based on 1 parameter (hydraulic conductivity ↔ intrinsic permeability)

What's new?

- Extension to other parameters like E , λ , α_s , c_p , ϕ
- Departure from rectangular to circular geometry
- Extension of plots to two more measures
- Spatial percentile plots

Governing equations – TRM (Pitz et al. 2023)

Heat balance:

$$\begin{aligned}
 & (\rho c_p)_{\text{eff}} \frac{dT}{dt} + L_0 \frac{d\theta_{\text{vap}}}{dt} - \text{div}(\boldsymbol{\lambda}_{\text{eff}} \text{grad } T) \\
 & + \text{div} \left(\frac{L_0 \mathbf{J}_G^W}{\rho_{GR}^W} \right) + \text{grad } T \cdot (c_{pL} \mathbf{A}_L + c_{p,\text{vap}} \mathbf{J}_G^W) = Q_T
 \end{aligned}$$

Mass balance:

$$\begin{aligned}
 & \rho_{LR} S_L (\alpha_B - \phi) \beta_{p,SR} \frac{dp_{LR}}{dt} - \rho_{LR} S_L (\alpha_B - \phi) \text{tr}(\boldsymbol{\alpha}_{T,SR}) \frac{dT}{dt} \\
 & + \phi \left((1 - S_L) \frac{d\rho_{GR}^W}{dt} + S_L \frac{d\rho_{LR}}{dt} \right) + (\rho_{LR} - \rho_{GR}^W) [\phi + p_{LR} S_L (\alpha_B - \phi)] \frac{dS_L}{dt} \\
 & + \rho_{LR} S_L \alpha_B \text{div} \left(\frac{d\mathbf{u}_S}{dt} \right) + \text{div}(\mathbf{A}_L^W + \mathbf{J}_G^W) = Q_H
 \end{aligned}$$

Momentum balance:

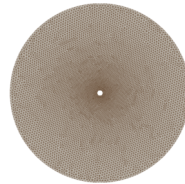
$$\text{div}(\boldsymbol{\sigma}^{\text{eff}} - \alpha_B \chi(S_L) p_{LR} \mathbf{I}) + \rho \mathbf{g} = \mathbf{0}$$

with

$$\dot{\boldsymbol{\sigma}}^{\text{eff}} = \mathbf{C} : (\dot{\boldsymbol{\epsilon}} - \dot{\boldsymbol{\epsilon}}_{\text{pl}} - \dot{\boldsymbol{\epsilon}}_{\text{th}} - \dot{\boldsymbol{\epsilon}}_{\text{sw}})$$

Model setup and specifics

- Simplified 2D mesh: $r = 50$ m
→ host rock (Opalinus clay)
- Circular heat source of $r = 1.5$ m
→ emplaced waste cell
- Anisotropic → Transverse isotropy
→ parallel and perpendicular to bedding plane
- Heterogeneous input parameters
→ Random Heterogeneous Field Generator Code
→ TU Chemnitz
- Uncertainty quantification using numerical modeling
→ TRM → OpenGeoSys
- Comparison of results with homogeneous, isotropic models



Simplified 2D mesh

Initial conditions:

$$T_0 = 15\text{ }^{\circ}\text{C}, p_0 = 2\text{ MPa}, u_{S0} = 0$$

Boundary conditions:

- Q_T (Neumann) at tunnel boundary
- $p = 0$ at tunnel boundary
- Normal $u_S = 0$ on outer boundary

CASE STUDIES

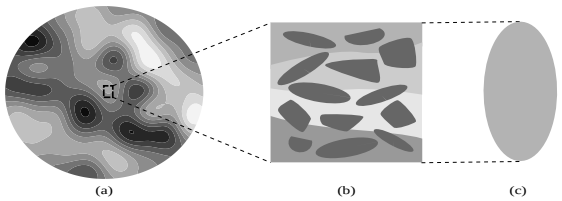
- > Let f be the parameter in question
- > f in this study -> λ, k, E
- > $f_{\perp} = a_f f_{\parallel}$, where a_f is a scaling factor

- Homogeneous, isotropic
-> $f_x = f_y = f_{\parallel}$
- Homogeneous, anisotropic
-> $f_x = f_{\parallel}, f_y = f_{\perp}$
- Heterogeneous, statistically isotropic, hydraulically isotropic
-> $f_x(\text{RF}) = f_y(\text{RF}) = f_{\parallel}$
- Heterogeneous, statistically isotropic, hydraulically anisotropic
-> $f_x(\text{RF}) = f_{\parallel}, f_y(\text{RF}) = f_{\perp}$

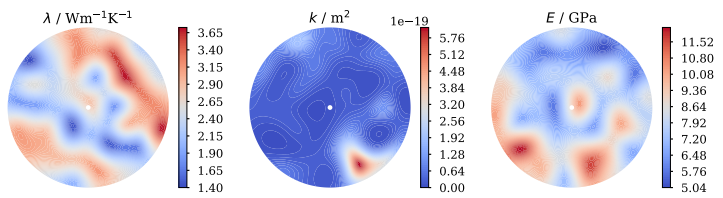
Work in progress

- Heterogeneous, statistically anisotropic, hydraulically isotropic
-> $f_x(\text{RF}_x) = f_{\parallel}, f_y(\text{RF}_y) = f_{\parallel}$
- Heterogeneous, statistically anisotropic, hydraulically anisotropic
-> $f_x(\text{RF}_x) = f_{\parallel}, f_y(\text{RF}_y) = f_{\perp}$

- Basic concept of the study

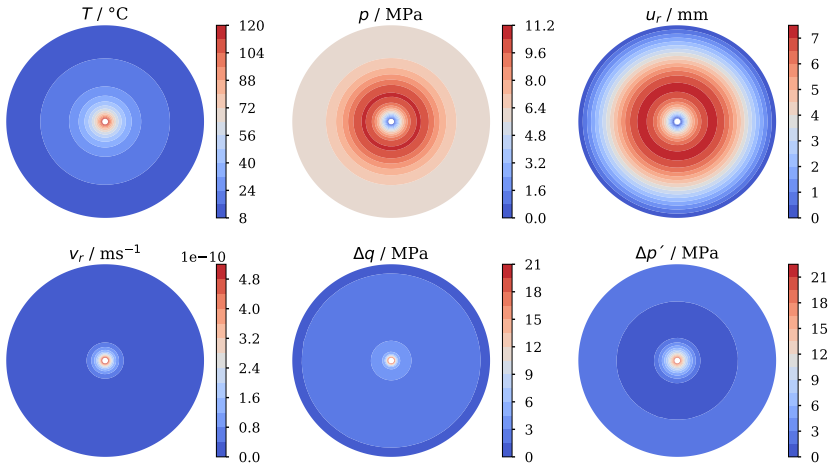


- Example of one random realisation

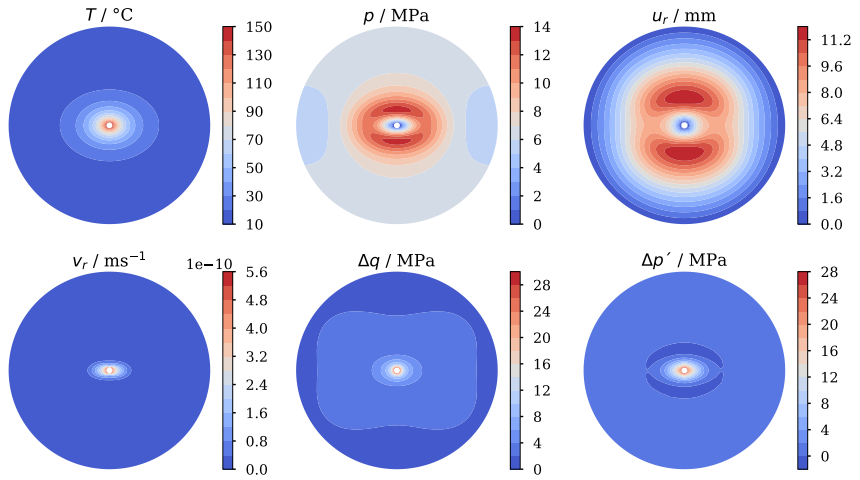


Inhomogeneity and anisotropy in THM simulations – Aqeel

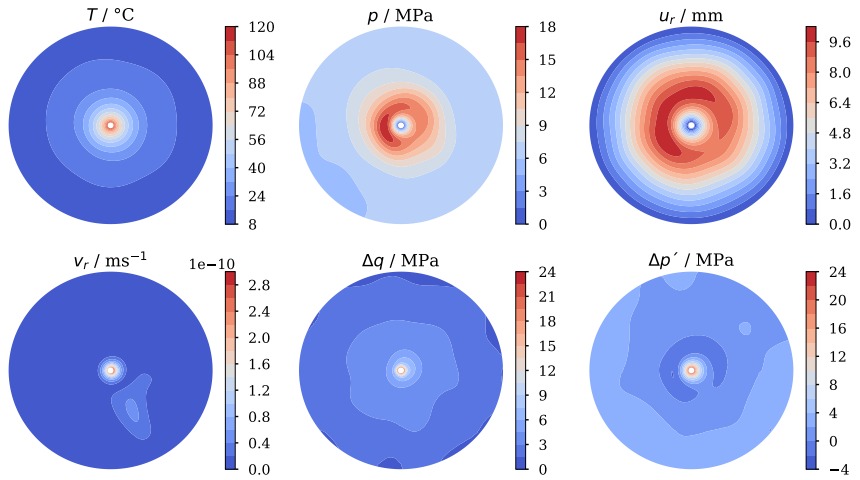
$\rightarrow \Delta q = \sqrt{\frac{3}{2} \sigma'_d : \sigma'_d} \quad \Delta p' = -\frac{1}{3} \sigma'_{ii}$
 Homogeneous, isotropic (reference) case



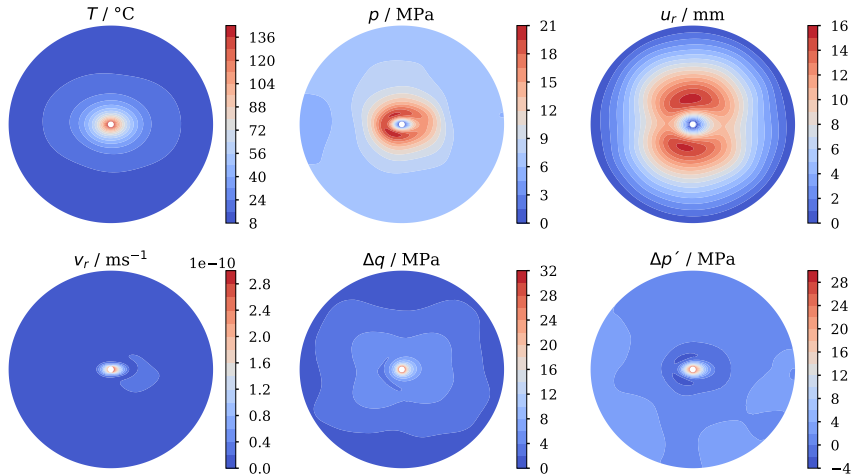
Homogeneous, anisotropic case



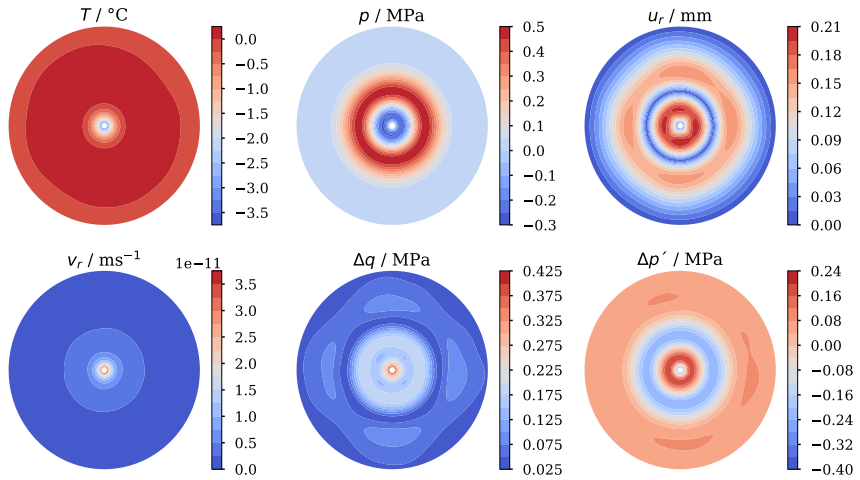
Heterogeneous, isotropic (single case)



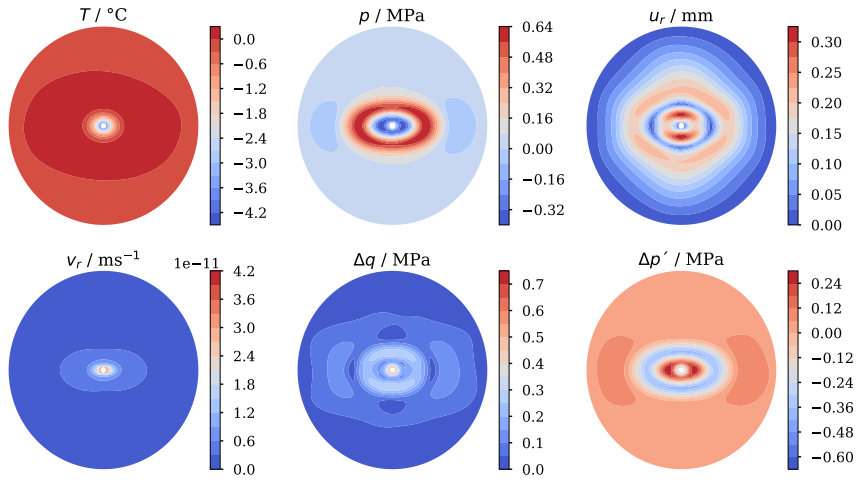
Heterogeneous, anisotropic (single case)



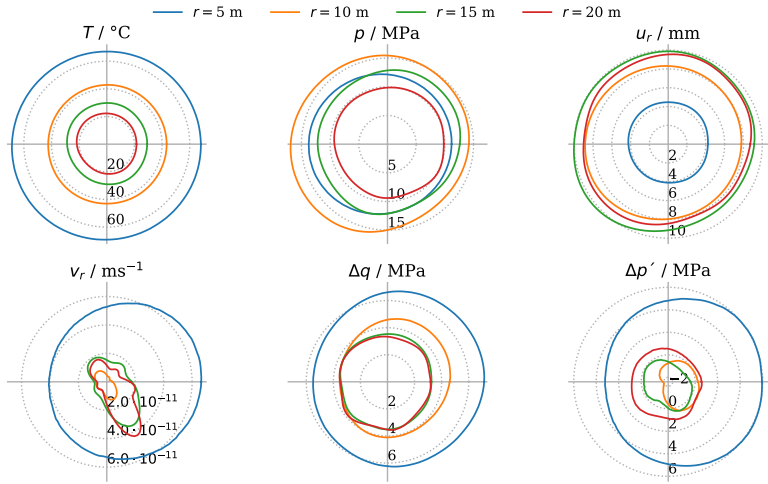
Diff. between hom. iso and mean of het. isotropic (needed?)



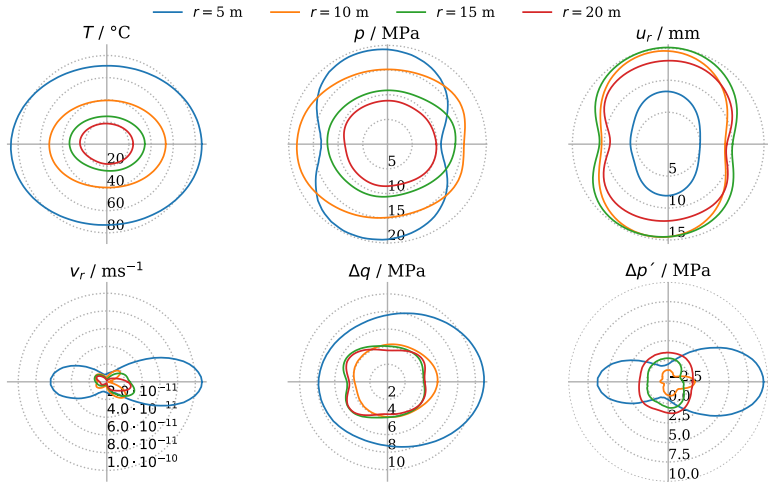
Diff. between hom. aniso and mean of het. anisotropic (needed?)



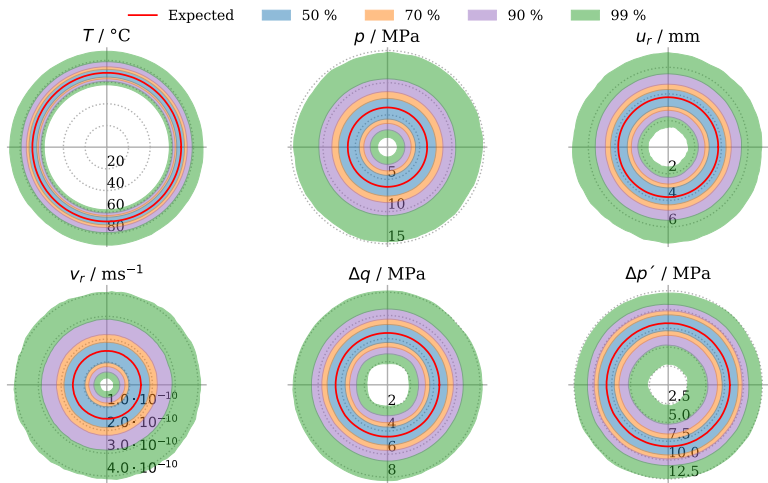
Heterogeneous, isotropic (single case)



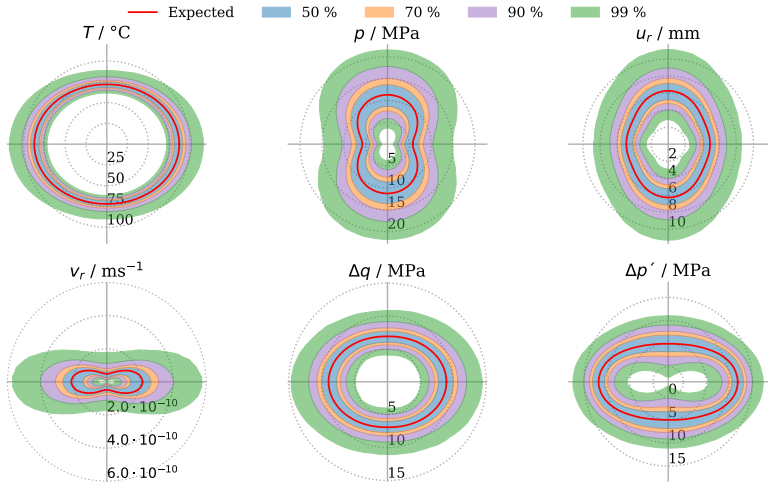
Heterogeneous, anisotropic (single case)



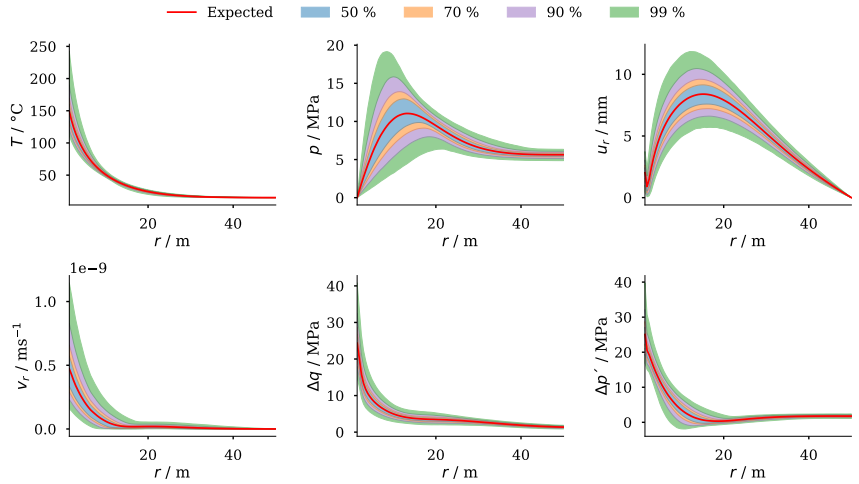
Heterogeneous, isotropic, percentiles at $r = 5$ m



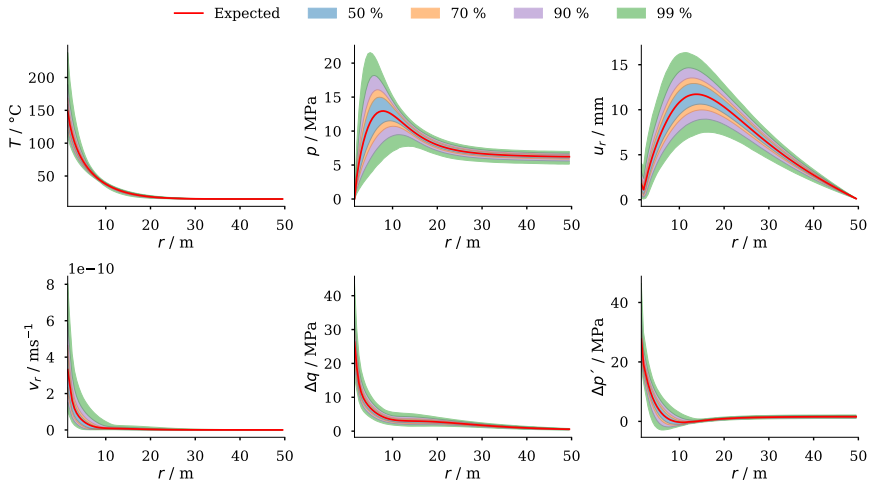
Heterogeneous, anisotropic, percentiles at $r = 5$ m



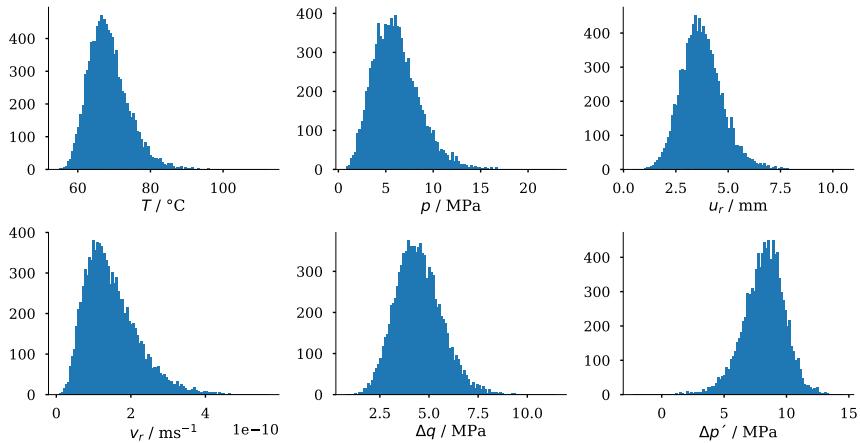
Heterogeneous, anisotropic, percentiles at $\theta = 0^\circ$



Heterogeneous, anisotropic, percentiles at $\theta = 90^\circ$



Heterogeneous, isotropic, histogram at $r = 5 \text{ m}$ & $\theta = 0^\circ$



Outlook

- Statistical anisotropy
→ Different correlation lengths
- Random anisotropy
→ $f_{\perp} \neq a_f f_{\parallel}$?
- Different boundary conditions (?)
- Unsaturated settings (?) (complex)
- Better ways to interpret results?
- Additional runs for min, mean, max for all 3 inputs

ACKNOWLEDGEMENTS

We would like to acknowledge the support from Bundesgesellschaft für Endlagerung and express our gratitude for making this project possible.



**BUNDESGESELLSCHAFT
FÜR ENDLAGERUNG**

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OUTLINE

`k1eme`: a C++ library to efficiently generate random fields for large-scale problems

- review of Karhunen-Loève expansion (KLE)
- numerical difficulties and our solutions in implementing KLE
- demo code

KARHUNEN-LOÈVE EXPANSION (KLE)

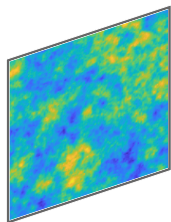
$$\mathbf{Z}(\mathbf{x}, \xi) \approx \sum_{i=1}^M \xi_i \sqrt{\lambda_i} \mathbf{f}_i(\mathbf{x})$$

λ_i and \mathbf{f}_i are eigenvalues and eigenfunctions, and ξ_i are draws from $\mathcal{N}(0, 1)$

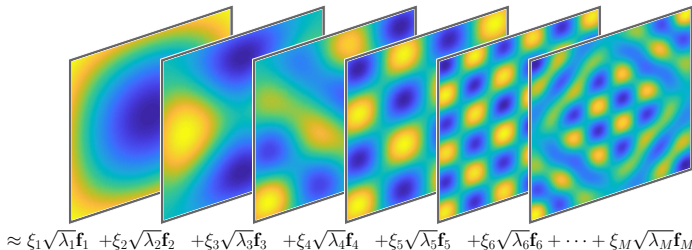
KARHUNEN-LOÈVE EXPANSION (KLE)

$$\mathbf{Z}(\mathbf{x}, \xi) \approx \sum_{i=1}^M \xi_i \sqrt{\lambda_i} \mathbf{f}_i(\mathbf{x})$$

λ_i and \mathbf{f}_i are eigenvalues and eigenfunctions, and ξ_i are draws from $\mathcal{N}(0, 1)$



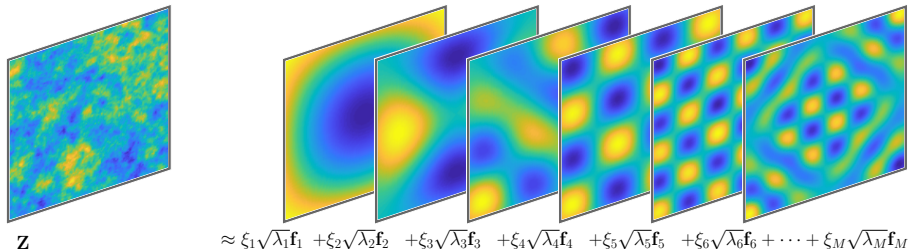
Z



KARHUNEN-LOÈVE EXPANSION (KLE)

$$\mathbf{Z}(\mathbf{x}, \xi) \approx \sum_{i=1}^M \xi_i \sqrt{\lambda_i} \mathbf{f}_i(\mathbf{x})$$

λ_i and \mathbf{f}_i are eigenvalues and eigenfunctions, and ξ_i are draws from $\mathcal{N}(0, 1)$



A random field Z represented as a set of $\{\xi_i\}$: dimension reduction

CALCULATION OF λ_I AND F_I

$$\mathbf{C}\mathbf{f}_i = \lambda_i \mathbf{M}\mathbf{f}_i$$

$$[\mathbf{C}]_{i,j} = \int_D \phi_j(\mathbf{x}) \int_D c(\mathbf{x}, \mathbf{y}) \phi_i(\mathbf{y}) d\mathbf{y} d\mathbf{x}$$

where ϕ is basis function and c is kernel/covariance function

CALCULATION OF λ_I AND F_I

$$\mathbf{C}\mathbf{f}_i = \lambda_i \mathbf{M}\mathbf{f}_i$$

$$[\mathbf{C}]_{i,j} = \int_D \phi_j(\mathbf{x}) \int_D c(\mathbf{x}, \mathbf{y}) \phi_i(\mathbf{y}) d\mathbf{y} d\mathbf{x}$$

where ϕ is basis function and c is kernel/covariance function

Difficulties

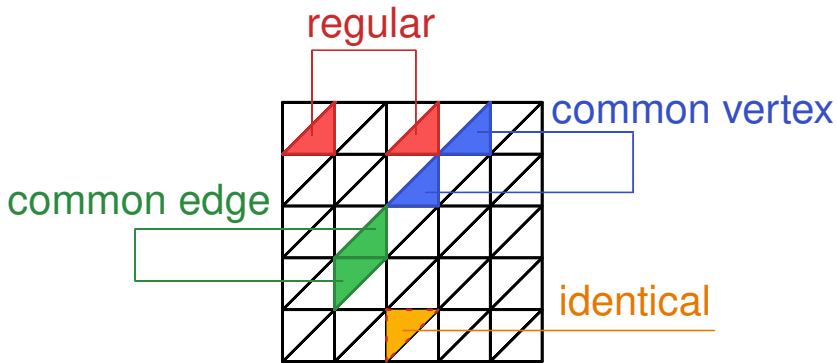
1. $[\mathbf{C}]_{i,j}$ involves integration of **singular** functions, i.e., $c(|\mathbf{x} - \mathbf{y}|)$
2. \mathbf{C} is **dense**, of size DOFs \times DOFs
 - storage is expensive
 - matrix-vector product is also expensive
3. **eigen** solver

Solutions

1. **Schauder-Schwab** quadrature from the BEM community to alleviate singularity
2. **hierarchical matrices**
3. **Thick-restart Lanczos**

SCHAUTER-SCHWAB QUADRATURE

$$[\mathbf{C}]_{i,j} = \int_D \phi_j(\mathbf{x}) \int_D c(\mathbf{x}, \mathbf{y}) \phi_i(\mathbf{y}) d\mathbf{y} d\mathbf{x}$$



SCHAUTER-SCHWAB QUADRATURE

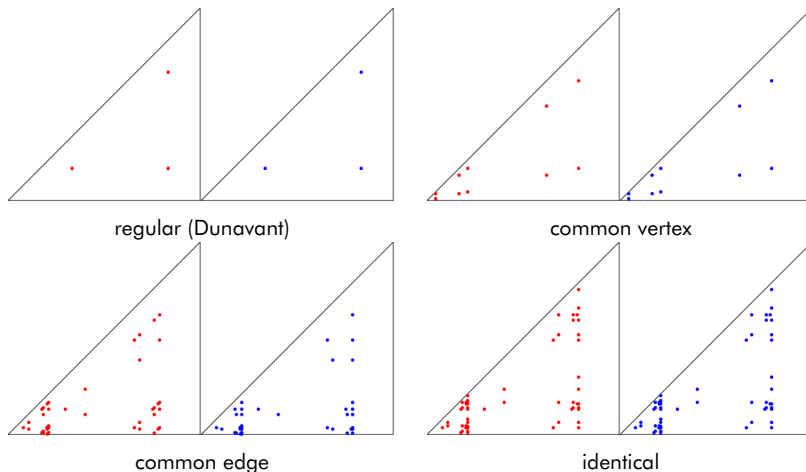


Fig. 9: Quadrature scheme on reference element pairs for 4 different cases

HIERARCHICAL MATRICES

Low-rank approximation of
far-field blocks

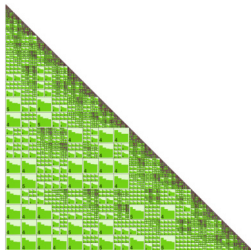


Fig. 10: Structure of a Hierarchical matrix

HIERARCHICAL MATRICES

Low-rank approximation of far-field blocks

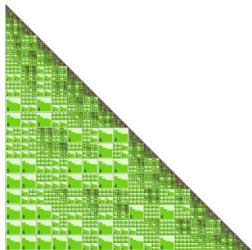


Fig. 10: Structure of a Hierarchical matrix

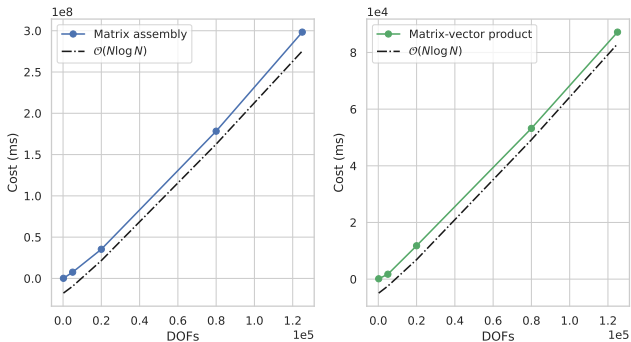


Fig. 11: Cost in terms of doing matrix assembly and matrix-vector product is reduced to $\mathcal{O} N \log N$ from N^2

CODE STRUCTURE

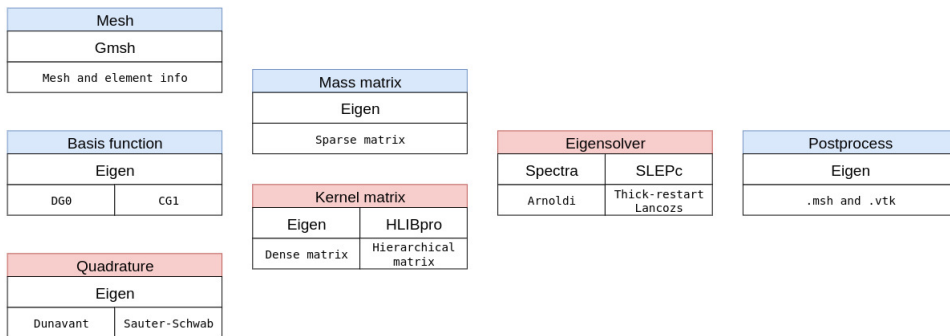


Fig. 12: Code structure

MINIMAL BUT COMPLETE DEMO

```
#include <kleme.h>
int main(int argc, char **argv)
{
    // parse mesh
    kleme::Mesh mesh(argv[1]);

    // define dofhandler to handle mesh and basis function
    kleme::DofHandler dofhandler(mesh, 0);

    // create and assemble mass matrix
    kleme::Mass m_matrix(&dofhandler);
    m_matrix.assemble_matrix();

    // prepare quadrature rule and kernel for later use
    // in assembling stiffness matrix
    kleme::Quadrature quad(mesh.get_dim(), 2);
    kleme::ExponentialKernel kernel(1, 0.1, 45, 0.5);

    // create and assemble stiffness matrix
    kleme::StiffnessHmatrix k_hmatrix(&dofhandler, &kernel, &quad);
    k_hmatrix.assemble_matrix();

    // create solver
    kleme::SLEPc_Solver solver_hmatrix(&k_hmatrix, &m_matrix);
    int no_of_eigens = 100;
    solver_hmatrix.solve(no_of_eigens);

    // postprocess
    kleme::Postprocess postprocess(&dofhandler);
    postprocess.write_vtk(slepcc_solver.eigen_vectors, "slepcc_eigens.vtk");

    return 0;
}
```

DOXYGEN DOCUMENTATION

kleme 0.3
Karhunen–Loève expansion made easy

Main Page Related Pages Namespaces ▾ Classes ▾ Files ▾

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kleme

- Example
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- Code structure**
- Performance
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- todo
- Namespaces
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- Files

kleme Documentation

kleme stands for **K**arhunen–**L**oève **e**xpansion **m**ade **e**asy. It is a C++ library for solving the integral eigen-value problem (IEVP) from discretizing the kernel operator with the Galerkin method.

Example

```
#include <kleme.h>
int main(int argc, char **argv)
{
    // parse mesh
    kleme::Mesh mesh(argv[1]);

    // define dofhandler to handle mesh and basis function
    kleme::DofHandler dofhandler(mesh, 0);

    // create and assemble mass matrix
    kleme::Mass m_matrix(&dofhandler);
    m_matrix.assemble_matrix();

    // prepare quadrature rule and kernel for later use
    // in assembling stiffness matrix
    kleme::Quadrature quad(mesh.get_dim(), 2);
    kleme::ExponentialKernel kernel(1, 0.1, 45, 0.5);

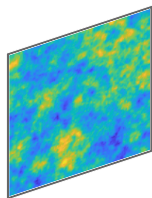
    // create and assemble stiffness matrix
    kleme::StiffnessMatrix k_hmatrix(&dofhandler, &kernel, &quad);
    k_hmatrix.assemble_matrix();

    // create solver
    kleme::SLEPC_Solver solver_hmatrix(&k_hmatrix, &m_matrix);
    int no_of_eigens = 100;
    solver_hmatrix.solve(no_of_eigens);

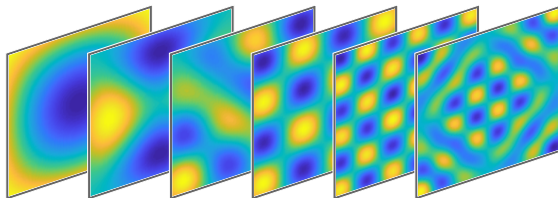
    // postprocess
    kleme::Postprocess postprocess(&dofhandler);
    postprocess.write_vtk(slepc_solver.eigen_vectors, "slepc_eigens.vtk");
}
```

CONCLUSIONS

- theories and techniques behind k1eme
- demonstration of the use
- working on further improvement of internal data structure and documentation



Z



$$\approx \xi_1 \sqrt{\lambda_1} \mathbf{f}_1 + \xi_2 \sqrt{\lambda_2} \mathbf{f}_2 + \xi_3 \sqrt{\lambda_3} \mathbf{f}_3 + \xi_4 \sqrt{\lambda_4} \mathbf{f}_4 + \xi_5 \sqrt{\lambda_5} \mathbf{f}_5 + \xi_6 \sqrt{\lambda_6} \mathbf{f}_6 + \dots + \xi_M \sqrt{\lambda_M} \mathbf{f}_M$$

Thanks!